

$$\hat{V}_a(s) = \sum \alpha_k e^{-s2kT} \quad \xrightarrow{2T=T} \quad = \sum \alpha_k \cdot e^{-skT} =$$

$$= \sum_{k=0}^{\infty} \alpha_k (e^{sT})^{-k}$$

Trans. vr. kont. filt

→ u vr. diskret.

Met. Jed. Imp Odz.

$$s \rightarrow z = e^{sT} \quad \leftarrow \begin{array}{l} T \dots \text{period} \\ \text{of imp.} \end{array}$$

$$\hat{V}_a(z) = \sum_{k=0}^{\infty} \alpha_k \cdot z^{-k}$$

↑
oznaci: impul. odziva sustava $V(z)$

bash. 10

↓
prijen. funk. VT
k vr. disk. dom.

poznak $e^{-sNz} = e^{-sN \cdot \frac{1}{z}} = (e^{st})^{N/2}$

poznak u VDD. je $z^{-N/2}$
za $N/2$ koraka

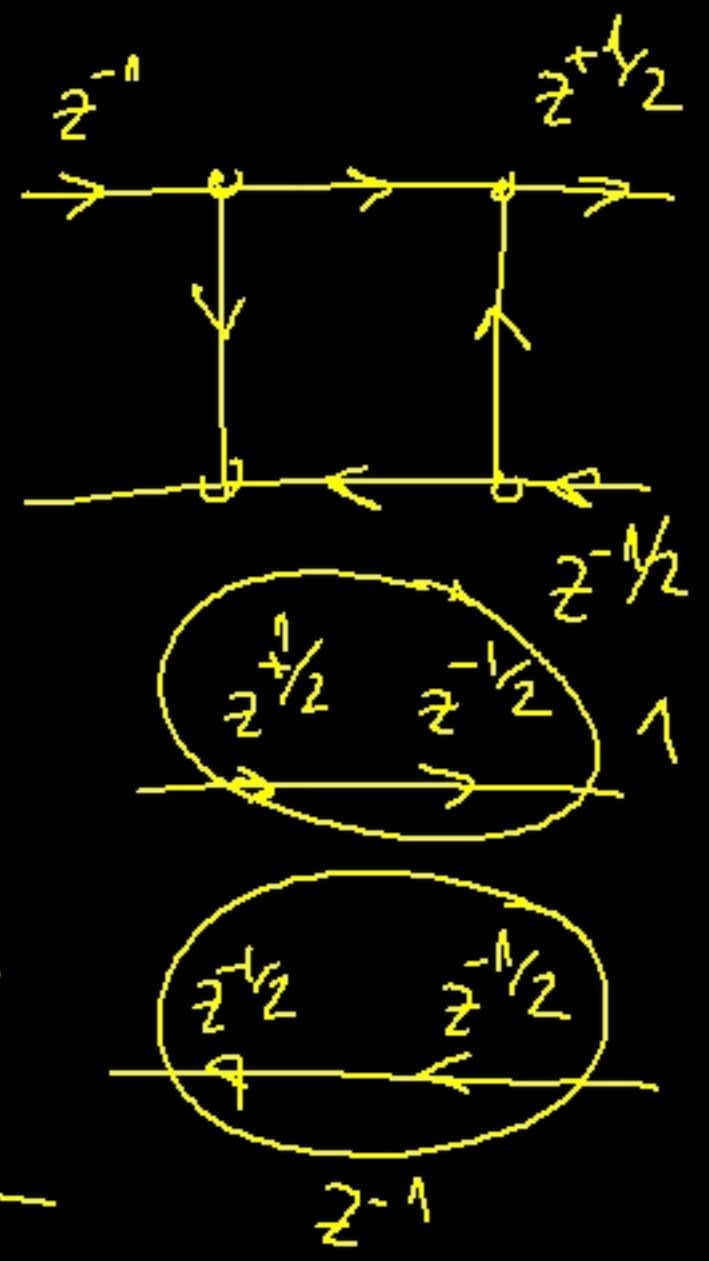
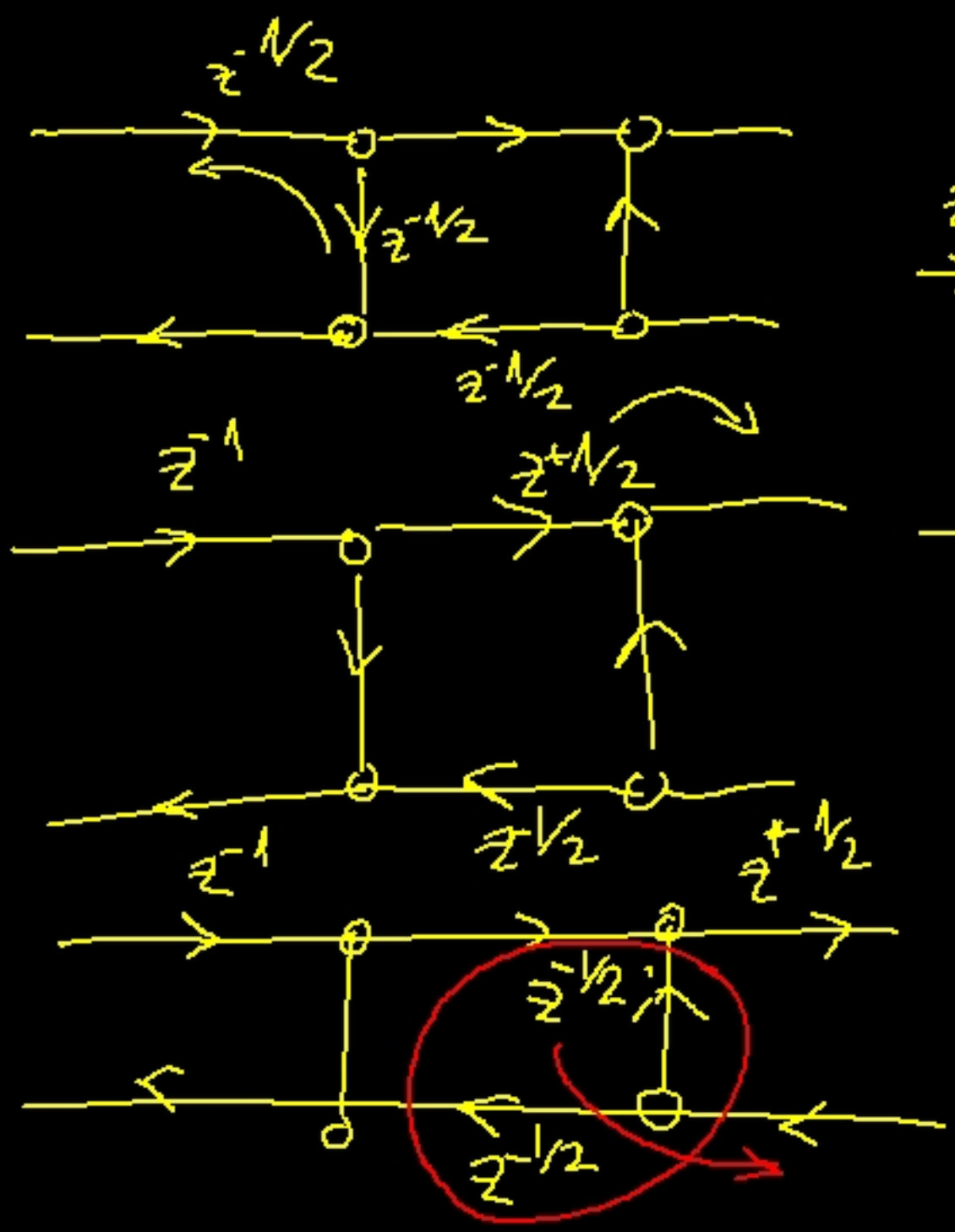
To tražimo

$$V_a(z) = \underbrace{z^{-N/2}}_{\text{poznak u vremenu}} \cdot \underbrace{\hat{V}_a(z)}_{\text{određuje formu. struk.}}$$

poznak u vremenu

određuje formu. struk.

linijski fazni član u s p.



$$r_k = \frac{A_{k+1} - A_k}{A_{k+1} + A_k}$$

factor reflection

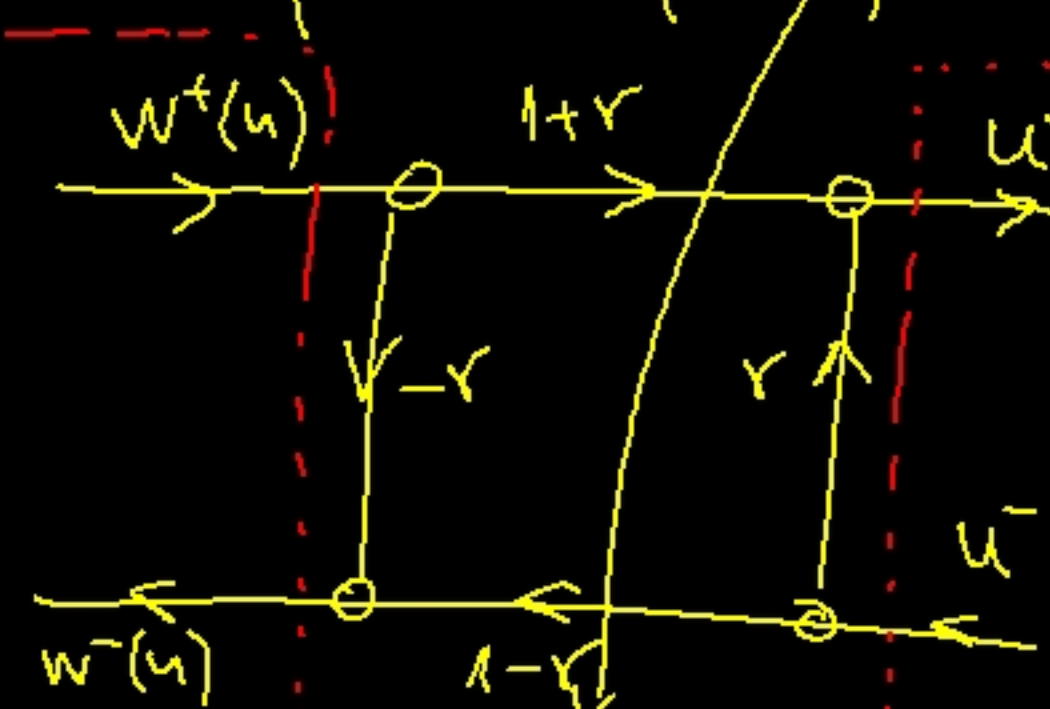
$$u^+(u) = (1+r)w^+(u) + r\bar{u}(u)$$

$$w^-(u) = (1-r)\bar{u}(u) - r w^+(u)$$

$$= w^+(u) + r w^+(u) + r\bar{u}(u)$$

$$= \bar{u}(u) - r\bar{u}(u) - r w^+(u)$$

к-ты
сцен



$$r w^+(u) = a^{(u)}$$

$$r \bar{u}(u) = b^{(u)}$$

$$u^+(u) = w^+(u) + a(u) + b(u)$$

$$w^-(u) = \bar{u}(u) - b(u) - a(u)$$

$$u^+(u) = w^+(u) + r(w^+(u) + \bar{u}(u))$$

$$w^-(u) = \bar{u}(u) - r(w^+(u) + \bar{u}(u))$$

$$U_L(z) = (1+r_L) z^{N/2} \cdot z^{-1} \cdot U_N^+(z)$$

$$U_N^-(z) = -r_L z^{-1} \cdot U_N^+(z)$$

$$U_N(z) = \begin{bmatrix} U_N^+(z) = z^{1-N/2} \cdot \frac{1}{1+r_L} \cdot U_L(z) \\ U_N^-(z) = z^{-N/2} \cdot \frac{-r_L}{1+r_L} \cdot U_L(z) \end{bmatrix}$$

$$U_N(z) = \frac{1}{1+r_L} z^{1-N/2} \begin{bmatrix} 1 \\ z^{-1} \cdot (-r_L) \end{bmatrix} U_L(z)$$

$$U_{k+1}^+(z) = U^+(z) \cdot \cancel{z^{-1}} \cdot (1+r_k) + r_k \cdot U_{k+1}^-(z)$$

$$U_k^-(z) = -r_k \cdot \cancel{z^{-1}} U_{k+1}^+(z) + (1-r_k) \cdot U_{k+1}^-(z)$$

$$r_k U_{k+1}^+(z) + (1+r_k) U_k^-(z) = \cancel{1-r_k^2}$$

$$\cancel{r_k^2 U_{k+1}^-(z)} + (1-r_k)(1+r_k) U_{k+1}^-(z)$$

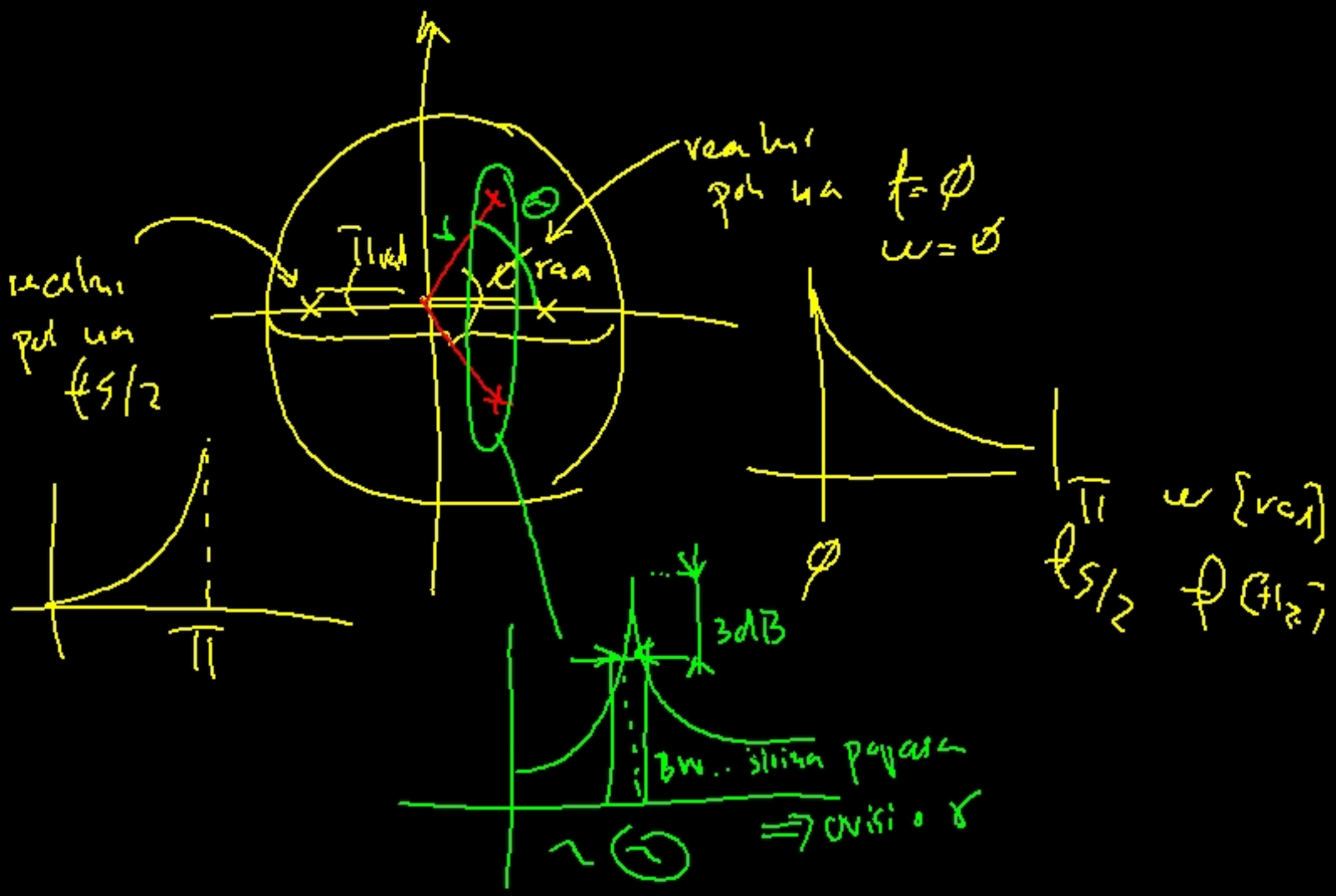
$$U_k^-(z) = \frac{1}{1+r_k} \left[-r_k U_{k+1}^+(z) + U_{k+1}^-(z) \right]$$

na pas.

$$U_1^+(z) = \frac{(1+r_G)}{2} U_G(z) + r_G \cdot U_1^-(z)$$

$$U_G(z) = \frac{2}{(1+r_G)} \left(U_1^+(z) - r_G U_1^-(z) \right)$$

$$U_G(z) = \frac{2}{(1+r_G)} \begin{bmatrix} 1 & -r_G \end{bmatrix} \begin{bmatrix} U_1^+(z) \\ U_1^-(z) \end{bmatrix} U_1(z)$$



$$r_G = 1$$

radi pojednostavljenja.

$$r_L = \frac{A_{N+1} - A_N}{A_{N+1} + A_N}$$

i $A_{N+1} = \infty \dots$ beskonačno duga cijev.

koji presjek A_{N+1} odgovara ideal. zahlij?

$$r_L = 1 \Rightarrow A_{N+1} = \infty$$

Za A_{N+1} konačan \Rightarrow
... imamo gužvithe

$$r_L \neq 1$$

$$r_L = r_N$$

zak. rel.
u spjuju
N-te cijevi VT
i N+1-ve cijevi koja
modelira prostor

Red sustava..

$$T = 2L$$

τ .. vrijeme proleta kroz cijev.

l .. ukupna duz. VT

N .. broj cijevi

dvima jednake cijevi $\Delta x = \frac{l}{N} \Rightarrow \tau = \frac{\Delta x}{c}$

$$\tau = \frac{l}{Nc} = \frac{T}{2} = \frac{1}{2 f_s} \quad f_s \dots \text{frek. otip.}$$

$$f_s = \frac{Nc}{2l} \quad \left| \begin{array}{l} c = 350 \text{ m/s} \\ l = 17.5 \text{ cm} \end{array} \right| = N \cdot 1000 \text{ [Hz]}$$

npri. ako je $f_s = 10 \text{ kHz}$

tada do 5 kHz koliko je $f_s/2$

imamo 5 formantata ω_c
prihl. razmak od 1000 Hz

\Rightarrow Svaki formant. traži 2 red sustava
par polova

\Rightarrow potrebno je $N=10$ polova za modeliranje
Svih 5 form.

veći f_s traži više N

manji $L \rightarrow$ veći razmak form. / pa je i niži red N
dovoljan za mod. svih form.

